Kuwait University College of Engineering and Petroleum



جامعة الكويت KUWAIT UNIVERSITY

ME417 CONTROL OF MECHANICAL SYSTEMS PART II: CONTROLLER DESIGN VIA STATE-SPACE LECTURE 1: STATE-SPACE REPRESENTATION

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Lecture Plan

- Objectives:
 - Introduction to modeling in the time domain
 - Treating the general state-space representation
 - Converting from state-space to transfer function and back
- Reading:
 - Nise: 3.1-3.6
- Practice Problems Included



- But why not just use transfer functions?
- Transfer functions are powerful. They help us understand dynamic systems behavior and they have a good set of tools (root-locus, bode plots)
- However, they are limited to
 - 1. Linear systems
 - Real world systems are often nonlinear
 - 2. Time-invariant systems
 - Systems may change their properties over time
- High order systems produce mathematically complex transfer functions
- A transfer function can only relate one input to one output
- Multi-degree of freedom systems must be decoupled if T.F. representation is desired



• The general state-space representation is

$$\dot{\mathbf{x}}(t) \in \mathcal{R}^{n \times 1} = f(\mathbf{x}, t, \mathbf{u}) = \mathbf{A}(\mathbf{x}, t) + \mathbf{B}(\mathbf{x}, t)$$
$$y(t) = \mathbf{C}(\mathbf{x}, t) + \mathbf{D}(\mathbf{x}, t)$$

f(x, t, u) is called the system model, which is a function of the system state x, time t and the input to the system u

- Note that f(x, t, u) correspond to the model function we use to simulate a general dynamic system numerically.
- The state-space representation can represent
 - Time-varying systems
 - Nonlinear dynamics
 - Multiple input and multiple outputs
 - Matrix representation for complex systems
 - Increasing system order increases matrix dimensions, rather than high order polynomial



 For linear time-invariant systems (the scope of this course) the representation is simplified to

> $\dot{x} = Ax + Bu$ y = Cx + Du

 $x \in \mathcal{R}^n$: State vector, $\dot{x} \in \mathcal{R}^n$: derivative of state vector,

- $\mathbf{A} \in \mathcal{R}^{n \times n}$: Constant System matrix, $\mathbf{B} \in \mathcal{R}^{n \times p}$: Constant Input matrix
- $\boldsymbol{u} \in \mathcal{R}^p$: Input vector,
- $y \in \mathcal{R}^m$: Output vector, $\mathbf{C} \in \mathcal{R}^{m \times n}$: Constant Output matrix,
- $\mathbf{D} \in \mathcal{R}^{n \times p}$: Constant Feedforward matrix
- $\in \mathcal{R}^{n \times n}$: denotes the matrix size is $n \times n$ and its values are real
- $\in \mathcal{R}^n$: denotes the vector size is n and its values are real
- *n*: Number of state variables, *p*: Number of inputs, *m*: Number of outputs



Linear Algebra Flash Refresher

• Matrix Addition/Subtraction

$$\mathbf{A}_{1} + \mathbf{A}_{2} = \mathbf{B} \Rightarrow \underbrace{\begin{bmatrix} 1 & -2 & 3 \\ 0 & 2 & -5 \\ 2 & 2 & 7 \end{bmatrix}}_{3x3} + \underbrace{\begin{bmatrix} -1 & 1 & 1 \\ 1 & 4 & 5 \\ 2 & -2 & 7 \end{bmatrix}}_{3x3} = \underbrace{\begin{bmatrix} 0 & -1 & 4 \\ 1 & 6 & 0 \\ 4 & 0 & 14 \end{bmatrix}}_{3x3}$$

• Matrix Scaling

$$c\mathbf{A} = \mathbf{B} \Rightarrow 3 \underbrace{\begin{bmatrix} 1 & 2 & 1 \\ 3 & 2 & 3 \\ 4 & 3 & 2 \end{bmatrix}}_{3x3} = \underbrace{\begin{bmatrix} 3 & 6 & 3 \\ 9 & 6 & 9 \\ 12 & 9 & 6 \end{bmatrix}}_{3x3}$$

Matrix Multiplication

$$\mathbf{A}x = y \Rightarrow \begin{bmatrix} 1 & 2 & 1 \\ 3 & 2 & 3 \\ 4 & 3 & 2 \end{bmatrix} \begin{bmatrix} 3 \\ 4 \\ 2 \\ 3x^3 \end{bmatrix} = \begin{bmatrix} 13 \\ 23 \\ 28 \\ 3x^1 \end{bmatrix}, \quad \mathbf{AB} = \mathbf{C} \Rightarrow \begin{bmatrix} 1 & 2 & 3 \\ 0 & 4 & 2 \\ 2 & 1 & 2 \end{bmatrix} \begin{bmatrix} 1 & 2 & 3 \\ 4 & 2 & 0 \\ 1 & 2 & 0 \\ 3x^3 \end{bmatrix} = \begin{bmatrix} 12 & 12 & 3 \\ 18 & 12 & 0 \\ 8 & 10 & 6 \end{bmatrix}$$



Linear Algebra Flash Refresher

• Matrix Inverse

$$\mathbf{A} \in \mathcal{R}^{n \times n}$$
, $\mathbf{A}^{-1} = \frac{adj(\mathbf{A})}{det(\mathbf{A})'}$, $\mathbf{A}\mathbf{A}^{-1} = \mathbf{I}$

• Matrix Adjugate

for
$$\mathbf{A} \in \mathcal{R}^{2 \times 2}$$
, $\mathbf{A} = \begin{bmatrix} a & b \\ c & d \end{bmatrix}$, $\operatorname{adj}(\mathbf{A}) = \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}$

• Matrix Determinant

for
$$\mathbf{A} \in \mathcal{R}^{2 \times 2}$$
, $\mathbf{A} = \begin{bmatrix} a & b \\ c & d \end{bmatrix}$, $\det(\mathbf{A}) = |\mathbf{A}| = ab - cd$

• Matrix Eigenvalues

 $\lambda_i \in C^n$ are the special constants of a matrix $\mathbf{A} \in \mathcal{R}^{n \times n}$, called the eigenvalues $\mathbf{A}x = \lambda_i x, Ax - \lambda_i x = (\mathbf{A} - \lambda_i \mathbf{I})x = 0$

The trivial solution is x = 0, while the nontrivial solution occurs if the determinant vanishes $det(\mathbf{A} - \lambda_i \mathbf{I}) = 0, i = 1, 2, ..., n$

The state-space representation

- Consider the mass-spring-damper mechanical system
- The equation of motion is: $M\ddot{x} + f_v\dot{x} + Kx = f(t) = u(t)$
- This is a second-order system, requiring 2 state variables
 - Corresponding to the two derivatives

$$\boldsymbol{x} = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} x \\ \dot{x} \end{bmatrix}$$

$$\dot{x} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} x_2 \\ (u(t) - f_v \dot{x} - Kx)/M \end{bmatrix} = \begin{bmatrix} x_2 \\ -f_v/Mx_2 - K/Mx_1 \end{bmatrix} + \begin{bmatrix} 0 \\ u(t)/M \end{bmatrix}$$





The state-space representation

$$\dot{\boldsymbol{x}} = \begin{bmatrix} 0 & 1 \\ -K/M & -f_{v}/M \end{bmatrix} \begin{bmatrix} x_{1} \\ x_{2} \end{bmatrix} + \begin{bmatrix} 0 \\ 1/M \end{bmatrix} \boldsymbol{u}(t) = \mathbf{A}\boldsymbol{x} + \mathbf{B}\boldsymbol{u}$$

$$y = x = x_1 = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \end{bmatrix} u(t) = \mathbf{C}x + \mathbf{D}u$$



$$\mathbf{A} \in \mathcal{R}^{2 \times 2} = \begin{bmatrix} 0 & 1 \\ -K/M & -f_v/M \end{bmatrix}, \quad \mathbf{B} \in \mathcal{R}^{2 \times 1} = \begin{bmatrix} 0 \\ 1/M \end{bmatrix}, \quad \xrightarrow{F(s)} \boxed{\frac{1}{Ms^2 + f_v s + K}} \xrightarrow{X(s)}$$

 $\mathbf{C} \in \mathcal{R}^{1 \times 2} = \begin{bmatrix} 1 & 0 \end{bmatrix}, \quad \mathbf{D} \in \mathcal{R} = \mathbf{0}$

• In this course $\mathbf{D} = 0$



Derive the dynamic model of the system shown in state-space form

Example 1





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• Given an nth order differential equation

$$a_n \frac{d^n x}{dt^n} + a_{n-1} \frac{d^{n-1} x}{dt^{n-1}} + \dots + a_1 \frac{dx}{dt} + a_0 x = f(t)$$

• We can write it as n simultaneous first-order differential equations:

$$\frac{dx_1}{dt} = a_{11}x_1 + a_{12}x_2 + \dots + a_{1n-1}x_{n-1} + a_{1n}x_n + b_1f(t)$$

$$\vdots$$

$$\frac{dx_i}{dt} = a_{i1}x_1 + a_{i2}x_2 + \dots + a_{in-1}x_{n-1} + a_{in}x_n + b_if(t)$$

$$\vdots$$

$$\frac{dx_n}{dt} = a_{n1}x_1 + a_{n2}x_2 + \dots + a_{nn-1}x_{n-1} + a_{nn}x_n + b_nf(t)$$



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 In state-space form, a general nth-order set of differential equations can be represented as:

$$\dot{\boldsymbol{x}} = \begin{bmatrix} \dot{x}_1 \\ \vdots \\ \dot{x}_n \end{bmatrix} = \begin{bmatrix} a_{11} & \cdots & a_{1n} \\ \vdots & \ddots & \vdots \\ a_{n1} & \cdots & a_{nn} \end{bmatrix} \begin{bmatrix} x_1 \\ \vdots \\ x_n \end{bmatrix} + \begin{bmatrix} b_1 \\ \vdots \\ b_n \end{bmatrix} f(t)$$

• The output y depends on what we are measuring. If state x_1 is the output then: $\begin{bmatrix} x_1 \end{bmatrix}$

$$\mathbf{y} = \begin{bmatrix} 1 & 0 & \cdots & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ \vdots \\ x_n \end{bmatrix} + 0$$

 Note that we use y(t) or c(t) interchangeably, to express the output. In statespace, it is common convention to use y(t) for the output.



From Transfer Function to State-Space

- To convert a transfer function into state space, we first convert it to differential equation form
- Given: $G(s) = \frac{C(s)}{U(s)} = \frac{b_0}{a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0}$, converting to diff. eq. • Gives: $a_n \frac{d^n c(t)}{dt^n} + a_n \frac{d^n c(t)}{dt^n} + \dots + a_1 \frac{dc(t)}{dt} + a_0 c(t) = b_0 u(t)$
- An nth order diff. eq. gives *n* states

$$\mathbf{x} = \begin{bmatrix} x_1 \\ \vdots \\ x_n \end{bmatrix} = \begin{bmatrix} c & dc/dt & \dots & d^{n-1}c/dt^{n-1} & d^nc/dt^n \end{bmatrix}^T$$

$$\dot{\mathbf{x}} = \begin{bmatrix} \dot{x}_1 \\ \vdots \\ \dot{x}_n \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & \dots & \dots & \dots & \dots \\ \dots & 0 & 1 & 0 & \dots & \dots & \dots \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \vdots \\ \dots & \dots & \dots & 0 & 1 & 0 \\ \dots & \dots & \dots & \dots & 0 & 1 \\ a_0/a_n & a_1/a_n & \dots & \dots & a_{n-2}/a_n & a_{n-1}/a_n \end{bmatrix} \begin{bmatrix} x_1 \\ \vdots \\ x_n \end{bmatrix} + \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1/a_n \end{bmatrix} u(t)$$

$$y = \begin{bmatrix} 1 & 0 & \dots & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ \vdots \\ x_n \end{bmatrix} + 0$$



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Part III: Controller Design via State-Space – L1

- The state-space form retrieved from the transfer function, is called a phase variable form
 - Note the off-diagonal identity matrix, and how all the coefficients are grouped in the nth row

$$A = \begin{bmatrix} 0 & 1 & 0 & \dots & \dots & \dots & \dots \\ \dots & 0 & 1 & 0 & \dots & \dots & \dots \\ \vdots & \vdots & \vdots & \ddots & \vdots & & \vdots \\ \dots & \dots & \dots & 0 & 1 & 0 \\ \dots & \dots & \dots & \dots & 0 & 1 \\ a_0/a_n & a_1/a_n & \dots & \dots & a_{n-2}/a_n & a_{n-1}/a_n \end{bmatrix}$$

- Unlike the state-space form retrieved from the equations of motion directly.
- Both the standard, and phase variable forms are valid representations





$$G(s) = \frac{Y(s)}{U(s)} = \frac{1}{s(s+3)+5}$$





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Part III: Controller Design via State-Space – L1



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From State Space to Transfer Function

• Given a state space representation of an LTI system, there is an analytical solution to expressing the system in transfer function form

• Given

 $\dot{x} = Ax + Bu$ y = Cx + Du

- Take the Laplace transform of both sides, we get sX(s) = AX(s) + BU(s)Y(s) = CX(s) + DU(s)
- Solving for **X**(*s*)

 $(sI - A)X(s) = BU(s) \implies X(s) = (sI - A)^{-1}BU(s)$, where I is the identity matrix



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• Substituting X(s) in Y(s)

$$Y(s) = \mathbf{C}((s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}U(s)) + \mathbf{D}U(s)$$
$$Y(s) = [\mathbf{C}((s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}) + \mathbf{D}]U(s)$$

- The term $\left[\mathbf{C}\left((s\mathbf{I} \mathbf{A})^{-1}\mathbf{B}\right) + \mathbf{D}\right]$, is the *transfer function matrix* $G(s) = \frac{Y(s)}{U(s)} = \left[\mathbf{C}\left((s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}\right) + \mathbf{D}\right]$
- The inverse term $(sI A)^{-1}$, can be computed as

$$(s\mathbf{I} - \mathbf{A})^{-1} = \frac{adj(s\mathbf{I} - \mathbf{A})}{det(s\mathbf{I} - \mathbf{A})}$$





From the following system given in state-space form, find the transfer function

Example 3

$$\dot{\boldsymbol{x}} = \begin{bmatrix} 5 & 3 \\ 2 & 3 \end{bmatrix} \boldsymbol{x} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} \boldsymbol{u}(t)$$
$$\boldsymbol{y} = \begin{bmatrix} 1 & 0 \end{bmatrix} \boldsymbol{x}$$



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Part III: Controller Design via State-Space – L1

Example 4 From the following system given in state-space form, represent the transfer function $G_2(s) = \frac{\Theta_2(s)}{M(s)}$ by the transfer function matrix, then compute using MATLAB $\dot{\boldsymbol{x}} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -2 & -3 & 2 & 3 \\ 0 & 0 & 0 & 1 \\ 2 & 3 & -2 & -3 \end{bmatrix} \boldsymbol{x} + \begin{bmatrix} 0 \\ 1 \\ 0 \\ 0 \end{bmatrix} \boldsymbol{u}(t), \ \boldsymbol{y} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \boldsymbol{x}, \quad \boldsymbol{x} = \begin{bmatrix} \theta_1 \\ \dot{\theta}_1 \\ \theta_2 \\ \dot{\theta}_2 \end{bmatrix}$ حامعة الكونن

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Part III: Controller Design via State-Space – L1

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- Note that the term det(sI A), is the denominator of the transfer function.
- In other words: it's the characteristic equation for the transfer function.
 - The roots of which are the poles of the system
- Note that the poles of the system are a function of the system matrix **A**
- So, stability can be evaluated by knowing the matrix **A**
- Remember that stability is defined in the context of the natural response (no input): $\dot{x} = Ax$
- Also note that the poles of the system are the eigenvalues λ_i of the matrix **A**



Is the following system stable?

 $\dot{\boldsymbol{x}} = \begin{bmatrix} 5 & 3 \\ 8 & 3 \end{bmatrix} \boldsymbol{x} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \boldsymbol{u}(t)$ $\boldsymbol{y} = \begin{bmatrix} 1 & 0 \end{bmatrix} \boldsymbol{x}$



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Example 5

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Part III: Controller Design via State-Space – L1

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